



## Surface Modification of Ni-YSZ Using Niobium Oxide for Sulfur-Tolerant Anodes in Solid Oxide Fuel Cells

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The surface of a dense Ni-yttria-stabilized zirconia (YSZ) anode for solid oxide fuel cells (SOFCs) was modified with niobium oxide ( $\text{Nb}_2\text{O}_5$ ) in order to achieve sulfur tolerance. Results suggest that  $\text{Nb}_2\text{O}_5$  was reduced to  $\text{NbO}_2$  under SOFC operating conditions, which has high electrical conductivity and catalytic activity toward hydrogen oxidation. The  $\text{NbO}_x$ -coated dense Ni-YSZ cermet anode showed sulfur tolerance when exposed to 50 ppm  $\text{H}_2\text{S}$  at  $700^\circ\text{C}$  over 12 h. Raman spectroscopy and X-ray diffraction analysis suggest that different phases of niobium sulfides ( $\text{NbS}_x$ ) were formed on the surfaces of niobium oxides. Furthermore, density of state (DOS) analysis of  $\text{NbO}_2$ ,  $\text{NbS}$ , and  $\text{NbS}_2$  indicates that the electronic structure of niobium sulfides are similar to that of  $\text{NbO}_2$ ; they are electrically conductive and catalytically active for hydrogen oxidation in  $\text{H}_2\text{S}$  containing fuels under the conditions studied.

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The advantages of solid oxide fuel cells (SOFCs) over other types of fuel cells include high energy efficiency and excellent fuel flexibility.<sup>1,2</sup> In particular, the possibility of direct utilization of fossil fuels and renewable fuels (e.g., biofuels) may significantly reduce the cost of SOFC technologies. However, it is known that these types of fuels contain many contaminants that may be detrimental to SOFC performance. For example, sulfur could deteriorate the functionality of Ni-based anodes under SOFC operating conditions.<sup>3</sup> Even though the desulfurization of fuels for the removal of sulfur species in some levels is available, the process becomes another source of high cost and system complexity in order to achieve low concentration of sulfur species. Thus, the design of sulfur-tolerant anode materials is essential to durability and commercialization of SOFCs.

Investigations into the mechanism of sulfur poisoning suggest<sup>4-6</sup> that the performance degradation of a Ni-yttria-stabilized zirconia (YSZ) anode can be attributed to sulfur adsorption on active surface sites and subsequent formation of two-dimensional (2D) surface nickel sulfides upon exposure to  $\text{H}_2\text{S}$ . The degree of the degradation in anode performance varies with operating conditions such as temperature, concentration of  $\text{H}_2\text{S}$ , and current density passing through the cell.<sup>4,7</sup> Although several alternative anode materials, such as  $\text{La}_{1-x}\text{Sr}_x\text{VO}_3$ ,<sup>8</sup>  $\text{La}_{1-x}\text{Sr}_x\text{TiO}_3$ ,<sup>9</sup> Y-doped  $\text{SrTiO}_3$ ,<sup>10</sup> and  $\text{CeO}_2$ -based anodes,<sup>11,12</sup> have shown some sulfur tolerance, none of these materials can satisfy all the practical requirements for SOFCs. For example, reasonable sulfur tolerance was observed with titanium oxide- and vanadium oxide-based anodes, but their electrochemical performances are relatively low. In the case of  $\text{Cu/CeO}_2/\text{YSZ}$ , tolerance to sulfur poisoning was observed up to 450 ppm  $\text{H}_2\text{S}$ ; however, ion impregnation must be used in the fabrication of the anode and thermal stability of copper should be taken into account. Recently, we studied the effect of surface modification<sup>13</sup> of Ni-YSZ anodes with  $\text{Nb}_2\text{O}_5$  coating on sulfur tolerance.

In this paper, we report our findings in surface modification of Ni-YSZ using niobium oxide for sulfur tolerance. In order to minimize experimental uncertainty in porous anodes, a dense Ni-YSZ anode was used for this study. Sulfur tolerance of Ni-YSZ coated with a thin film of niobium oxide was investigated experimentally and computationally in order to understand the mechanism of sulfur tolerance.

### Experimental

**Phase analysis and electrical property of reduced  $\text{Nb}_2\text{O}_5$ .**— To investigate the phase stability of  $\text{Nb}_2\text{O}_5$  under operating conditions of the anode, reduced powder was prepared by reducing  $\text{Nb}_2\text{O}_5$  powder in  $\text{H}_2$  (UHP grade, Airgas) at  $750^\circ\text{C}$  for 24 h, and the resulting phase was confirmed as  $\text{NbO}_2$  using X-ray diffraction (XRD) (Philips, PW-1800). The electrical conductivity of the reduced phase was measured using impedance spectroscopy in a two-electrode configuration in the temperature range from 600 to  $850^\circ\text{C}$  with  $50^\circ\text{C}$  increments in  $\text{H}_2$  after a  $\text{Nb}_2\text{O}_5$  pellet sintered at  $1250^\circ\text{C}$  for 5 h was reduced under the same condition. A porous Pt cathode was formed on the other side of the electrolyte by brush painting and subsequent firing at  $850^\circ\text{C}$  for 3 h of Pt paste (Heraeus). The impedance system consisting of a potentiostat/galvanostat (EG&G, 273A) and a lock-in amplifier (Princeton Applied Research) interfaced with a computer was used.

**Preparation of dense Ni-YSZ and surface modification with  $\text{Nb}_2\text{O}_5$ .**— As shown in Fig. 1, two-layered cells consisting of dense YSZ (Tosoh) and Ni-YSZ were prepared using a copressing and cosintering method in 4%  $\text{H}_2$  balanced with Ar at  $1400^\circ\text{C}$  for 3 h. The thicknesses of the YSZ (8 mol % Y-doped zirconia) electrolyte and the Ni-YSZ anode were about 400 and 100  $\mu\text{m}$ , respectively. For the dense Ni-YSZ anode, 20 wt % of metal Ni powder (Alfa Aesar, 3–5  $\mu\text{m}$ ) was used to avoid significant distortion of the cells due to mismatch of the coefficient of thermal expansion. The surface of dense Ni-YSZ was confirmed to be conductive using an ohmmeter with a well-distributed Ni network in the dense structure. Reactive sputtering was used to deposit a  $\sim 500$  nm thick  $\text{Nb}_2\text{O}_5$  layer on the top of the dense Ni-YSZ surface. A small area on the edge of the

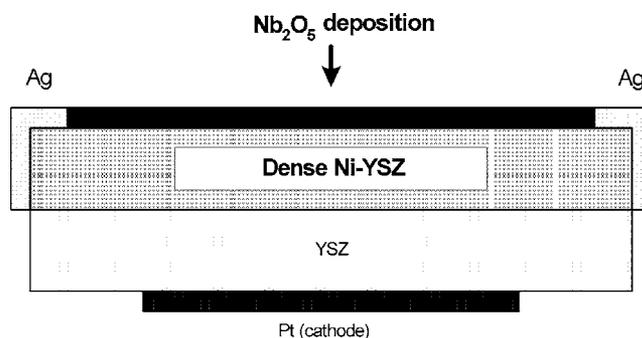


Figure 1. Schematic of dense Ni-YSZ structure with  $\text{Nb}_2\text{O}_5$  coating for sulfur tolerance test.

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dense Ni-YSZ layer was masked for current collection as shown in Fig. 1. A Ag current collector was used and directly contacted with Ni-YSZ through the masked area in order to reduce any contribution between the current collector and the modified surface with Nb<sub>2</sub>O<sub>5</sub> coating.

**Electrochemical characterization and sulfur poisoning test.**— The electrochemical behavior of functional cells of Pt/YSZ/dense Ni-YSZ with Nb<sub>2</sub>O<sub>5</sub> coating was characterized by measuring peak power density and impedance spectra. The impedance was typically measured in the frequency range of 1 MHz to 0.01 Hz using a lock-in amplifier (Princeton Applied Research) and a potentiostat/galvanostat (EG&G, 273A) interfaced with a computer. The fuel cell performance was acquired using the CorrWare software. For sulfur poisoning tests, the anode was exposed to H<sub>2</sub> containing 50 ppm H<sub>2</sub>S at a flow rate of 40 mL/min while the cathode was exposed to ambient air. The experimental apparatus was as described elsewhere.<sup>4</sup> The sulfur tolerance tests were conducted in a potentiostatic mode, i.e., monitoring the cell current at a constant cell voltage, as the fuel was switched from H<sub>2</sub> to 50 ppm H<sub>2</sub>S containing fuel or vice versa. Each cell was tested in clean H<sub>2</sub> at 700°C for several days until the performance was stabilized before a small amount of H<sub>2</sub>S was introduced.

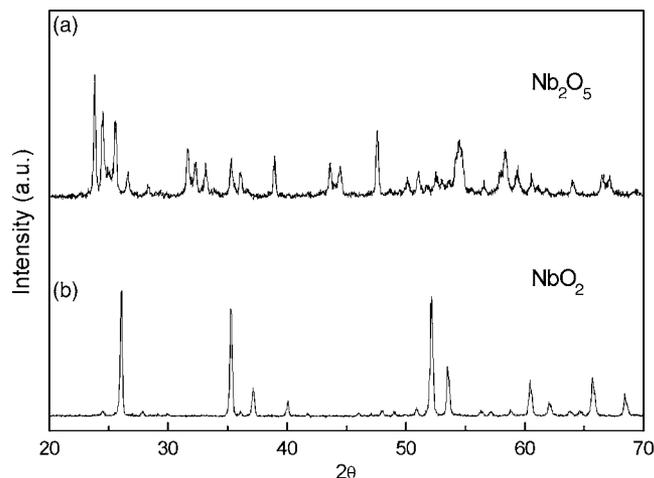
**Surface analysis.**— To investigate the surface change in a H<sub>2</sub>S containing fuel, fine Nb<sub>2</sub>O<sub>5</sub> powder with a large surface area was prepared by evaporating the solution of Nb(HC<sub>2</sub>O<sub>4</sub>)<sub>4</sub>·6H<sub>2</sub>O at 150°C. The collected powder was calcinated at 500°C for 5 h and reduced in dry H<sub>2</sub> at 800°C for 24 h. Then, the powder was exposed to 100 ppm H<sub>2</sub>S balanced with H<sub>2</sub> at 700°C for 15 h. The reaction chamber was cooled down in Ar, instead of 100 ppm H<sub>2</sub>S, to avoid further reaction of the powder with H<sub>2</sub>S at lower temperatures. The powder samples were examined using Raman microspectroscopy (Renishaw 2000, 514 nm laser, 1 mW) and XRD before and after exposure to 100 ppm H<sub>2</sub>S, and after regeneration in clean H<sub>2</sub>.

### Computational

The Vienna Ab Initio Simulation Package (VASP),<sup>14-16</sup> at the density functional theory (DFT) level with periodic conditions, was used for the quantum-chemical calculations.

**Electronic structure calculations.**— The generalized gradient approximation<sup>17</sup> with the Perdew-Wang 1991 (PW91) exchange-correlation functional<sup>18</sup> and the projector-augmented wave method,<sup>19,20</sup> a method combining the accuracy of augmented plane waves with the cost-effective pseudopotentials implemented in VASP, was applied. This plane wave expansion included all plane waves with their kinetic energies smaller than the chosen cutoff energy of 400 eV to ensure the convergence with respect to the basis set and the efficiency of the computational cost. The Brillouin-zone (BZ) integration was sampled with  $0.05 \times 2\pi$  (1/Å) spacing in reciprocal space by the Monkhorst-Pack scheme.<sup>21</sup> The crystal structures of the interest oxides and sulfides were initially optimized and compared to XRD observations to validate the computational methodology. On the basis of optimized structures, the density of state (DOS) calculations were performed for electronic structure study.

**Phase diagram calculations.**— To take into consideration of the environmental effects under the condition for fuel cell operation, the Gibbs free energy  $G(T,p)$  of the whole system was calculated as a function of temperature and pressure from the DFT results, as described elsewhere.<sup>22-26</sup> The Gibbs free energy for a solid phase was approximated by the DFT computed energy,  $G_{\text{surface}}(T,p) \approx E_{\text{surface}}^{\text{DFT}}$  because of the relatively small variation, <10 meV, in a wide range of temperatures (<1500 K) and pressures (<100 atm).<sup>22,26</sup> The Gibbs free energy of the gas phase O<sub>2</sub> was obtained by adding the thermodynamic corrections from the



**Figure 2.** XRD spectra of Nb<sub>2</sub>O<sub>5</sub> power (a) before and (b) after reduction in dry H<sub>2</sub> at 750°C for 24 h.

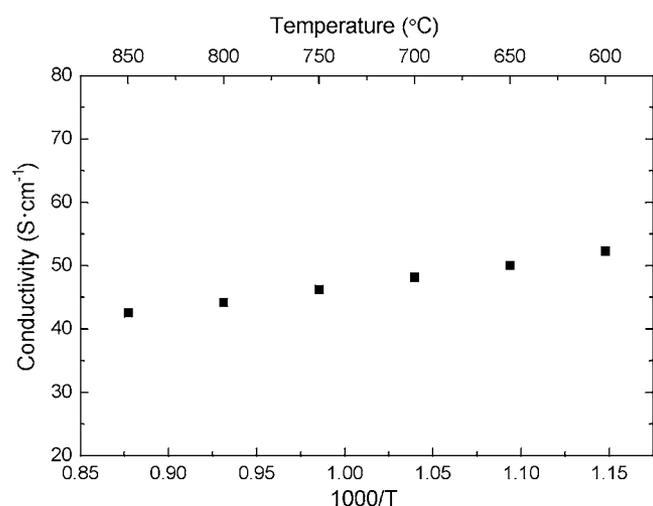
database<sup>27</sup> to the DFT values:  $G_{\text{O}_2}(T,p) = E_{\text{O}_2}^{\text{DFT}} + \Delta H_{\text{O}_2}(T,p^0) + RT \ln(p_{\text{O}_2}/p^0)$ , where  $H_{\text{O}_2}$  is the standard enthalpy of O<sub>2</sub> molecule and  $R$  is the gas constant.

**Vibrational analysis.**— The crystal phonons were computed from the optimized geometries by applying the finite displacement approach.<sup>28,29</sup> The interatomic force-constant matrix (Hessian matrix) was derived from a set of calculations on a periodically repeated super cell that contains several unit cells. At the starting point, all atoms were put at the equilibrium position. Then each atom was slightly displaced and the forces on all atoms were calculated. These computed forces were proportional to the interatomic force constants times the displacement. The full Hessian matrix was obtained by considering all symmetry-inequivalent displacements and truncated due to the finite size of the super cell as it rapidly decayed to zero with increasing interatomic separations. The frequencies as a function of the normal modes were obtained via matrix diagonalization and computed at the  $\Gamma$ -point of the BZ in order to allow comparison to the spectroscopic observations.

### Results and Discussion

**Phase analysis of Nb<sub>2</sub>O<sub>5</sub> under reducing conditions.**— As shown in Fig. 2, Nb<sub>2</sub>O<sub>5</sub> was reduced to NbO<sub>2</sub> after being immersed in dry H<sub>2</sub> at 750°C for one day. Thus, Nb<sub>2</sub>O<sub>5</sub> is not stable under fuel cell operating conditions, and the actual phase will be either Nb<sub>2</sub>O<sub>5</sub> or NbO<sub>2</sub>, depending on the partial pressure of oxygen. It is known that the reduced phases of Nb<sub>2</sub>O<sub>5</sub> have high electrical conductivities while their ionic conductivities are negligible.<sup>30,31</sup> To determine the temperature dependence of electrical property of NbO<sub>2</sub>, we measured the electrical conductivity of NbO<sub>2</sub> in pure H<sub>2</sub>. As shown in Fig. 3, NbO<sub>2</sub> displayed typical metallic behaviors.

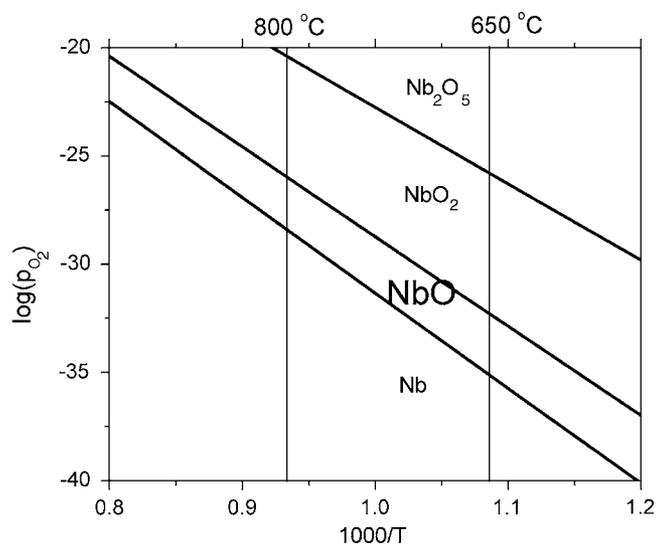
The result of NbO<sub>2</sub> formation was also confirmed with the predicted phase diagram from Gibbs free energy calculations, as shown in Fig. 4. For pressure effect, the oxygen-rich oxides appear in the higher oxygen partial pressures. For the temperature effect, the oxidized phases are more stable at low temperatures because the oxidation processes are all exothermic:  $\text{Nb} + \frac{1}{2}\text{O}_2 \rightarrow \text{NbO}$ ,  $\Delta E = -4.26$  eV;  $\text{NbO} + \frac{1}{2}\text{O}_2 \rightarrow \text{NbO}_2$ ,  $\Delta E = -3.74$  eV; and  $\text{NbO}_2 + \frac{1}{2}\text{O}_2 \rightarrow \frac{1}{2}\text{Nb}_2\text{O}_5$ ,  $\Delta E = -1.70$  eV. Under the experimental condition at 750°C, the Nb<sub>2</sub>O<sub>5</sub> will reduce to NbO<sub>2</sub> when  $p_{\text{O}_2} < 10^{-22}$  atm at thermoequilibrium. In addition, the observed electrical behavior of NbO<sub>2</sub> is consistent with the prediction from the DOS analysis; as shown in Fig. 5, only Nb<sub>2</sub>O<sub>5</sub> in the Nb–O systems is an insulator and has a wide bandgap around the Fermi level.



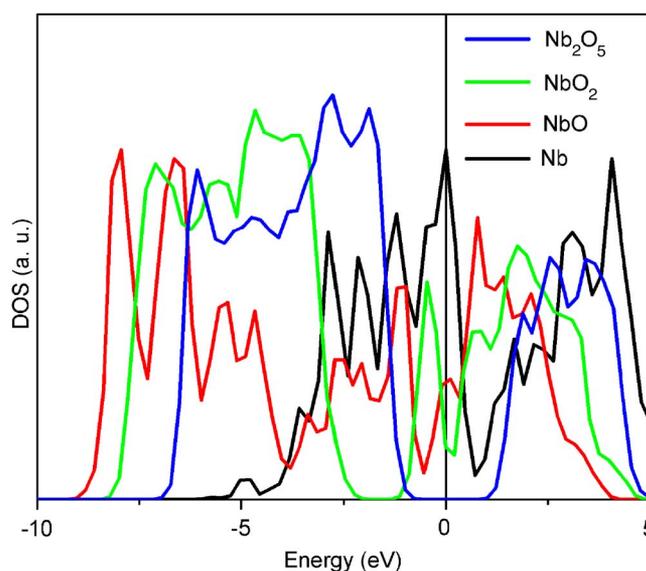
**Figure 3.** Conductivity of  $\text{NbO}_2$  reduced from  $\text{Nb}_2\text{O}_5$  as a function of temperature in dry  $\text{H}_2$  measured by two-electrode ac measurement.

*Effect of  $\text{Nb}_2\text{O}_5$  coating on electrochemical performances.*— Shown in Fig. 6a are the power densities as a function of current density for cells of Pt/YSZ/dense Ni-YSZ with and without  $\text{Nb}_2\text{O}_5$  coating in dry  $\text{H}_2$  at  $700^\circ\text{C}$ . The peak power density was  $\sim 23 \text{ mW/cm}^2$  for the cell without  $\text{Nb}_2\text{O}_5$  coating and  $\sim 49 \text{ mW/cm}^2$  for the cell with  $\text{Nb}_2\text{O}_5$  coating on the dense Ni-YSZ anode. This enhancement in power output resulted from the reduced  $\text{NbO}_2$  with high electrical conductivity under operating conditions; the conductive  $\text{NbO}_2$  coatings may create additional triple phase boundaries for the electrochemical reactions. In addition, the good catalytic activity of niobium oxides for  $\text{H}_2$  dissociative adsorption claimed by previous studies<sup>31-33</sup> may also attribute to the enhanced power density of  $\text{Nb}_2\text{O}_5$  modified Ni-YSZ anode.

Shown in Fig. 6b are the impedance spectra of the two cells under open-circuit conditions. The observed increase in power density was due mainly to the decrease in the interfacial polarization resistance from about  $15$  to  $7 \Omega \text{ cm}^2$ , which may be attributable to the improved catalytic activity of  $\text{NbO}_2$  or the increased triple-phase boundary length due to the addition of  $\text{NbO}_2$  to the dense Ni-YSZ anode.

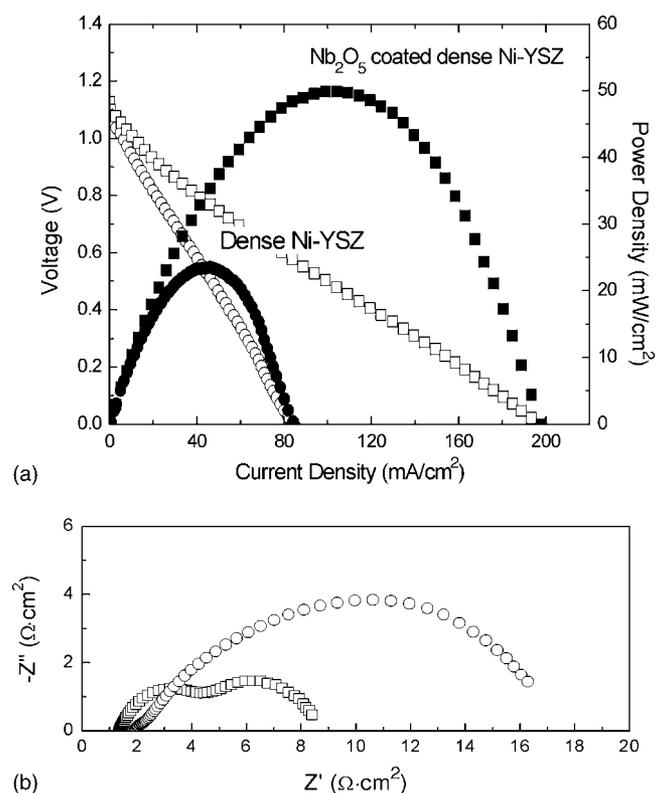


**Figure 4.** Phase diagram of the Nb-O system.



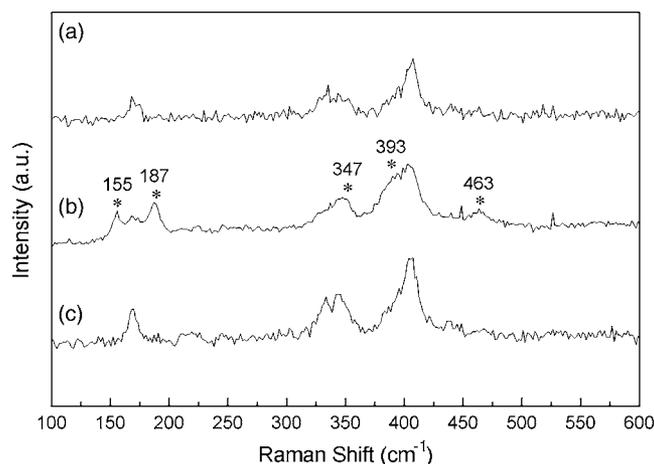
**Figure 5.** (Color online) Total DOS of  $\text{Nb}_2\text{O}_5$ ,  $\text{NbO}_2$ ,  $\text{NbO}$ , and  $\text{Nb}$ .

*Sulfur tolerance test.*— Shown in Fig. 7 is the sulfur tolerance test of Pt/YSZ/dense Ni-YSZ with  $\text{Nb}_2\text{O}_5$  coating. The  $\text{Nb}_2\text{O}_5$ -coated Ni-YSZ anode was exposed to 50 ppm  $\text{H}_2\text{S}$  after the cell performance was stabilized in  $\text{H}_2$  at  $700^\circ\text{C}$ . The operating temperature was kept at  $700^\circ\text{C}$  to observe a significant sulfur-poisoning effect. The change of current density as a function of time by switching the fuel from  $\text{H}_2$  to 50 ppm  $\text{H}_2\text{S}$  balanced with  $\text{H}_2$  shows a slight, quick drop when  $\text{H}_2\text{S}$  is introduced, but, immedi-



**Figure 6.** Comparison of (a) power densities as a function of current densities and (b) impedance spectra of Pt/YSZ/dense Ni-YSZ with (squares) and without (circles)  $\text{Nb}_2\text{O}_5$  coating in dry  $\text{H}_2$  at  $700^\circ\text{C}$ .



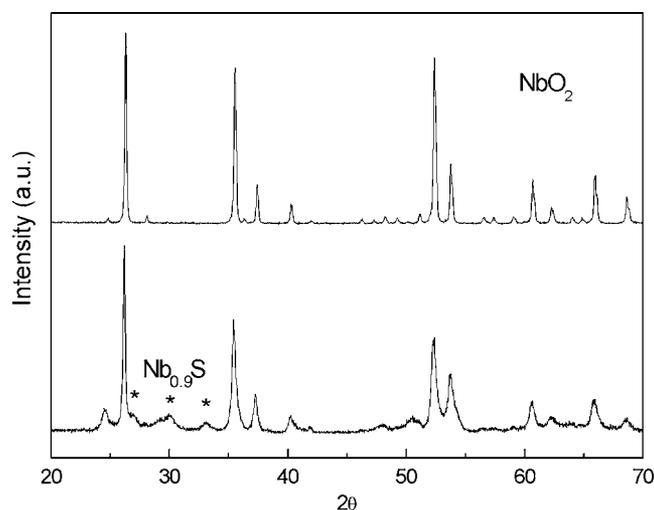


**Figure 10.** Raman spectra of (a)  $\text{Nb}_2\text{O}_2$  powder after reduction in  $\text{H}_2$  at  $800^\circ\text{C}$  for 24 h, (b)  $\text{Nb}_2\text{O}_2$  powder after being exposed to 100 ppm  $\text{H}_2\text{S}$  balanced with  $\text{H}_2$  at  $700^\circ\text{C}$  for 15 h, and (c)  $\text{Nb}_2\text{O}_5$  powder after regeneration in  $\text{H}_2$  at  $700^\circ\text{C}$  for 15 h.

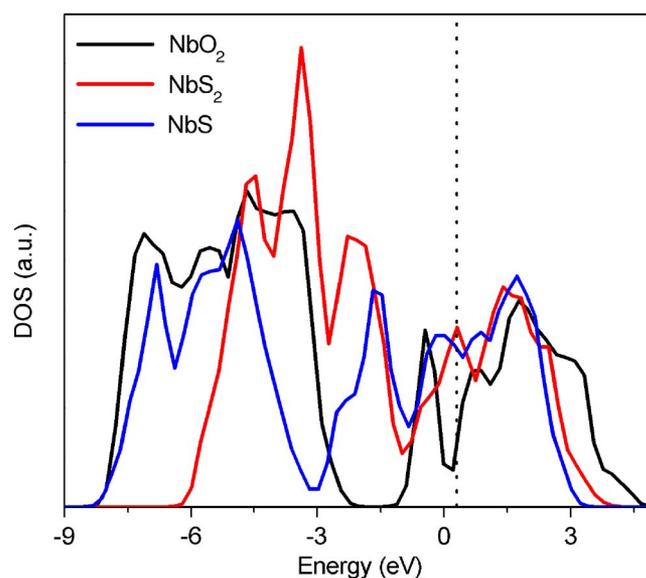
The different phases observed from Raman ( $\text{NbS}_2$ ) and XRD ( $\text{Nb}_{0.9}\text{S}$ ) spectroscopy can be attributed to the detection limits between them. Raman spectroscopy is more sensitive to the surface phases because of the limited penetration depth of visible light, while XRD has much greater penetration depth, probing the bulk properties. As a result, the sulfur-rich compound ( $\text{NbS}_2$ ), detected from Raman spectroscopy, is expected to appear in the top layers when  $\text{H}_2\text{S}$  directly reacts with the surface. The deeper layers, detected by XRD, have a Nb-rich stoichiometry because the formation depends on the bulk diffusion of sulfur atoms. In both cases, ni-

**Table I.** Experimentally observed and computed Raman frequencies of  $\text{NbS}_2$ .

	Modes	Expt.	Calc.	Ref.
$\text{NbS}_2$	$A_1$	463		458, <sup>23</sup> 462 <sup>24</sup>
		393	394	382 <sup>22</sup> , 386 <sup>23,24</sup>
	$E$	347	349	329, <sup>22</sup> 330, <sup>23</sup> 322 <sup>24</sup>
		187		191 <sup>24</sup>
		155		150, <sup>22</sup> 158 <sup>23</sup>



**Figure 11.** XRD spectra of (a)  $\text{Nb}_2\text{O}_2$  powder after reduction in  $\text{H}_2$  at  $800^\circ\text{C}$  for 24 h and (b)  $\text{Nb}_2\text{O}_2$  powder after being exposed to 100 ppm  $\text{H}_2\text{S}$  balanced with  $\text{H}_2$  at  $700^\circ\text{C}$  for 15 h.

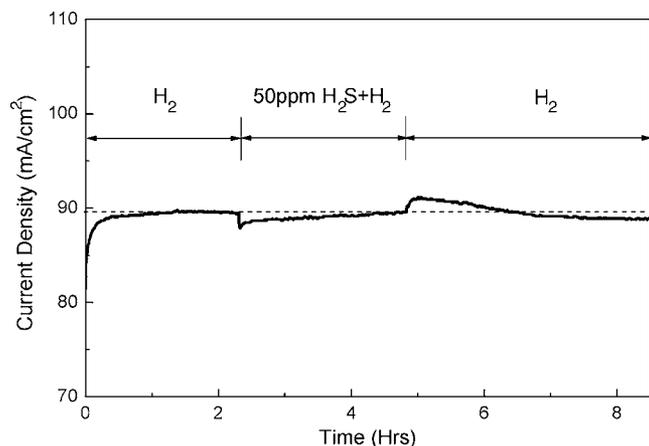


**Figure 12.** (Color online) DOS analysis of before ( $\text{NbO}_2$ ) and after ( $\text{NbS}_2$ ) sulfur exposure.

mium sulfides were formed by the reaction of  $\text{NbO}_2$  with  $\text{H}_2\text{S}$  on the surface. However, in the functional cell tests, no evidence of sulfide formation was identified from the modified anode surface after exposure to 50 ppm  $\text{H}_2\text{S}$ , probably due to the oxidative environment in the presence of water and oxygen ions transferred from the electrolyte in a functional cell.

**DOS analysis.**— The degradation of the electrochemical performance corresponds to the changes of conductivity and catalytic ability of the anode materials when sulfides are formed in the sulfur-poisoning process. The conductivity can be attributed to the bandgap calculations, and the catalytic ability of  $\text{H}_2$  oxidation corresponds to the band structure of the materials. These intrinsic properties can be understood from the electronic structure (DOS) analysis. Shown in Fig. 12 is the DOS analysis of the  $\text{NbO}_2$  (before  $\text{H}_2\text{S}$  exposure) and the possible sulfides,  $\text{NbS}$  and  $\text{NbS}_2$  (after  $\text{H}_2\text{S}$  exposure). The results show that no obvious bandgaps were found around the Fermi level in the sulfides, indicating that the sulfide-covered anode is still conductive for the electrochemical reactions. In addition, comparing the DOS of the phases without ( $\text{NbO}_2$ ) and with sulfur exposure ( $\text{NbS}$  and  $\text{NbS}_2$ ), all of them have similar DOS distribution, indicating that the catalytic activity of the sulfides is as good as that of  $\text{NbO}_2$ . Thus, the DOS analysis predicts that both  $\text{NbO}_2$  and niobium sulfides ( $\text{NbS}$  and  $\text{NbS}_2$ ) are conductivity and catalytically active.

**Surface regeneration.**— To investigate the regeneration process on the modified anode with  $\text{Nb}_2\text{O}_5$ , the current density was monitored in a short-term test carried out at  $700^\circ\text{C}$  with fuel transitions, from  $\text{H}_2$  to 50 ppm  $\text{H}_2\text{S}$  with  $\text{H}_2$  and vice versa, as shown in Fig. 13. After the sulfur tolerance test with 50 ppm  $\text{H}_2\text{S}$ , the fuel was switched back to pure  $\text{H}_2$  and the current density was restored to the initial value in the measurement. Similar to the result in the sulfur tolerance test in Fig. 7, the current density in Fig. 13 shows a quick drop when  $\text{H}_2\text{S}$  is introduced and slowly increased over the following 3 h. Furthermore, in the regeneration process when 50 ppm  $\text{H}_2\text{S}$  was switched to pure  $\text{H}_2$ , the current density increased abruptly and started to decrease slowly, followed by stable current density. The initial drop in  $\text{H}_2\text{S}$  may be attributable to the sulfur adsorption on the Ni surfaces that are not covered by  $\text{NbO}_2$ . The abrupt increase in the regeneration process with  $\text{H}_2$  reintroduction could be considered as the desorption of the adsorbed sulfur. The slow increase of current density in 50 ppm  $\text{H}_2\text{S}$  and slow decrease in pure  $\text{H}_2$  can be explained by the surface changes, the formation of niobium sulfides,



**Figure 13.** Variation of current density depending on fuels of Pt/YSZ/dense Ni-YSZ with Nb<sub>2</sub>O<sub>5</sub> coating in dry H<sub>2</sub> and 50 ppm H<sub>2</sub>S balanced with H<sub>2</sub> at 700°C after 0.5 V is applied.

of NbO<sub>2</sub> on Ni-YSZ by the interaction with H<sub>2</sub>S, as identified in Raman spectroscopy and XRD. The formation and decomposition of niobium sulfides can be taken into account for the slow changes. This behavior is not seen in the conventional Ni-YSZ anode, indicating that the changes of current density in H<sub>2</sub>S can be attributed to the surface modification with Nb<sub>2</sub>O<sub>5</sub>.

### Conclusions

We have demonstrated the possibility of surface modification for sulfur tolerance using a dense Ni-YSZ anode coated with a layer of niobium oxide. The increase in peak power density for a cell with a surface modified dense Ni-YSZ anode was due mainly to the decrease in the interfacial polarization resistance originating in the niobium oxide coating. It was found that Nb<sub>2</sub>O<sub>5</sub> was reduced to NbO<sub>2</sub> on exposure to H<sub>2</sub>, as predicted from the computed phase diagram. The metallic behavior of NbO<sub>2</sub> was confirmed by both conductivity measurement and theoretical calculation.

In the sulfur tolerance test, the cell current remained relatively constant on exposure to 50 ppm H<sub>2</sub>S for over 12 h. The observed excellent sulfur tolerance of a Nb<sub>2</sub>O<sub>5</sub>-coated Ni-YSZ anode is attributed to the good catalytic activity for H<sub>2</sub> oxidation of the surface sulfides formed on the niobium oxide surface in low concentrations of H<sub>2</sub>S.

Furthermore, the observed slow changes in cell current as the fuel was switched from clean H<sub>2</sub> to H<sub>2</sub> containing 50 ppm H<sub>2</sub>S (or vice versa) can be explained by the corresponding phase changes of the niobium oxide on Ni-YSZ, as identified using Raman spectroscopy and XRD analyses. The formation and decomposition of niobium sulfides can be taken into account for the slow changes and correspond to the Raman spectrum change before and after H<sub>2</sub>S

exposure. However, in the functional cell tests, no evidence of sulfide formation was observed after the exposure to 50 ppm H<sub>2</sub>S, due probably to limited sulfide formation because of the inflow of oxygen ions from the cathode under active fuel cell operation.

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